

## Purifier capacity, and efficiency

D.Shuman July/1/2001

Matheson gas gives N<sub>2</sub> max impurity level for 5N Xe as <3 ppmv      ppmv := 10<sup>-6</sup>

$C_{N_2_{Xe}} := 3 \cdot \text{ppmv}$  This is a volumetric density ratio, which is a mole ratio, not a mass ratio

no ratio is given for N<sub>2</sub> in 5N Ar, but N<sub>2</sub> in 5N He is same value, for N<sub>2</sub> in 5N Kr it is 10ppmv  
assume 5N Ar has 3ppmv N<sub>2</sub>

The Pureguard purifier claims it delivers <1ppb N<sub>2</sub> for 30 SLPM ( once through flow) for one year, this flow rate is  
as defined elsewhere one standard cubic cm of gas is:

$$\text{scc} = 4.464 \times 10^{-5} \text{ mol} \quad \text{so -->} \quad \text{SLPM} := 10^3 \text{ scc} \cdot \text{min}^{-1} \quad \text{SLPM} = 7.44 \times 10^{-4} \text{ mol} \cdot \text{s}^{-1}$$

molar gas flow rate:

$$q_{\text{gas}} := 30 \text{ SLPM} \quad q_{\text{gas}} = 0.022 \text{ mol} \cdot \text{s}^{-1}$$

at 15 bar pressure, room temp., this is a volumetric flow rate:

$$v_{\text{gas}} := q_{\text{gas}} \cdot \frac{(R \cdot 293 \text{ K})}{15 \text{ bar}} \quad v_{\text{gas}} = 0.036 \text{ L} \cdot \text{s}^{-1}$$

If we assume that we cannot increase the molar flow through the getter (high flow restriction? damage?) then  
we have an initial molar removal rate:

$$q_{N_2 t0} := C_{N_2_{Xe}} \cdot q_{\text{gas}} \quad q_{N_2 t0} = 6.696 \times 10^{-8} \text{ mol} \cdot \text{s}^{-1}$$

this removal rate is constant for a once through gas system, so we can estimate capacity, assuming the  
purifier is saturated after this:

$$Q_{N_2} := q_{N_2 t0} \cdot 1 \text{ yr}$$

$$Q_{N_2} = 2.113 \text{ mol} \quad Q_{N_2} = 4.734 \times 10^4 \text{ scc} \quad M_{a_N} := 14 \text{ gm} \cdot \text{mol}^{-1}$$

$$M_{N_2} := Q_{N_2} \cdot M_{a_N} \quad M_{N_2} = 29.6 \text{ gm}$$

Assume we have a total quantity of Xe in vessel :

density at 15 bara

$$M_{Xe} = 147.9 \text{ kg} \quad N_{Xe} := M_{Xe} \cdot M_{a_{Xe}}^{-1} \quad N_{Xe} = 1.088 \times 10^3 \text{ mol} \quad \rho_{Xe} := .091 \frac{\text{gm}}{\text{cm}^3} \quad V_{Xe} := M_{Xe} \cdot \rho_{Xe}^{-1}$$

This would have, at 5N purity :

$$N_{N_2} := N_{Xe} \cdot C_{N_2_{Xe}} \quad N_{N_2} = 3.263 \times 10^{-3} \text{ mol}$$

The similarly priced SAES getter, rated at 5 SLPM for 1 year would only get 1/6 of this, but would still have  
plenty of capacity for 5N Xe. Our EXe is likely more pure than 5N

Since impurity concentration removal rate will go down, as gas gets cleaner (because we cannot increase  
molar flow rate beyond rated value), time to reach a certain impurity level (assuming first, no outgassing of  
components) is

molar rate of change = molar rate of inflow - molar rate of outflow.

$$\frac{d}{dt} Q := 0 - q_{\text{gas}}$$

$$\frac{d}{dt} Q := -\frac{Q}{V} \cdot v_{\text{gas}} \quad \text{where } V \text{ is vessel volume and } Q \text{ is amount of } N_2 \text{ in vessel, in mol}$$

$$\frac{1}{Q} dQ := -\frac{v_{\text{gas}}}{V} dt$$

integrating both sides

$$\ln(Q) - \ln(Q_0) := -\frac{t \cdot v_{\text{gas}}}{V} \text{ or } \ln\left(\frac{Q}{Q_0}\right) := \frac{-t \cdot v_{\text{gas}}}{V} \text{ or } Q := Q_0 \cdot e^{\frac{-t \cdot v_{\text{gas}}}{V}}$$

time to reach 1 ppb N2

$$t_{1\text{ppb}} := \ln\left(\frac{10^{-9}}{3 \cdot 10^{-6}}\right) \cdot \frac{-V_{\text{Xe}}}{v_{\text{gas}}} \quad t_{1\text{ppb}} = 4.156 \text{ day} \quad \text{or 25 days for SAES getter}$$

Adding in outgassing from internal components and area, we will need the general form of solution for 1st order ODE. First we need to quantify an outgassing rate which will change as concentration in plastic goes down over time. However, we can see qualitatively, that impurity level in the gas may rise before it falls, if initial outgassing rate is higher than initial removal rate.

to be continued...